

Numerical investigations of the spherical flow regimes induced by constant-rate pumping tests

Anouck FERROUD, Romain CHESNAUX, Silvain RAFINI

anouck.ferroud@gmail.com

1. Introduction



1.1 Terms and concepts

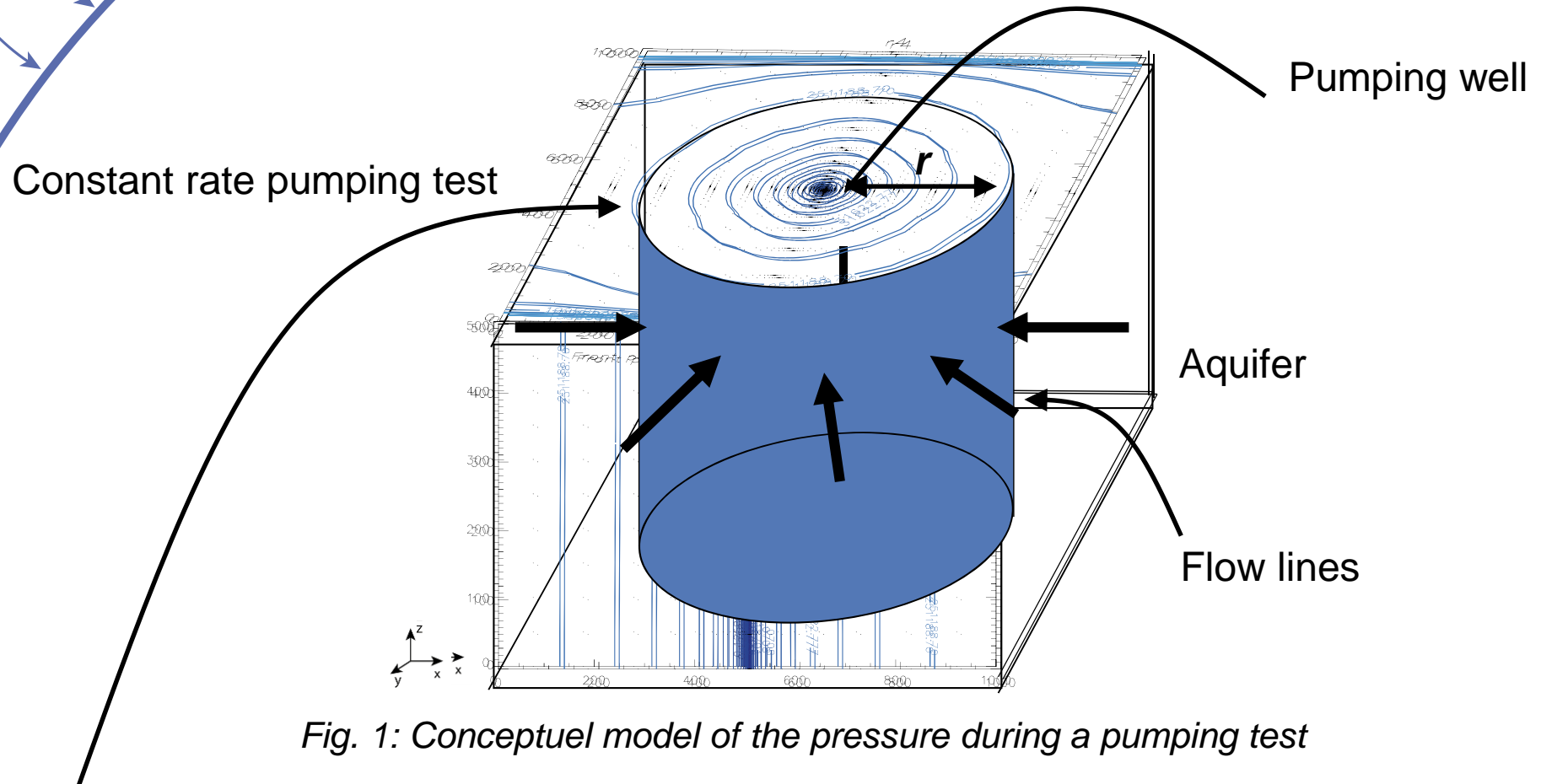


Fig. 1: Conceptuel model of the pressure during a pumping test

Pressure front pulse (or pressure wave)

Radial distance r

Cross flow area $A(r)$ (equipotential surface)

1.2 Constant rate pumping tests : diagnostic tools

" The old way " *

Drawdown
s

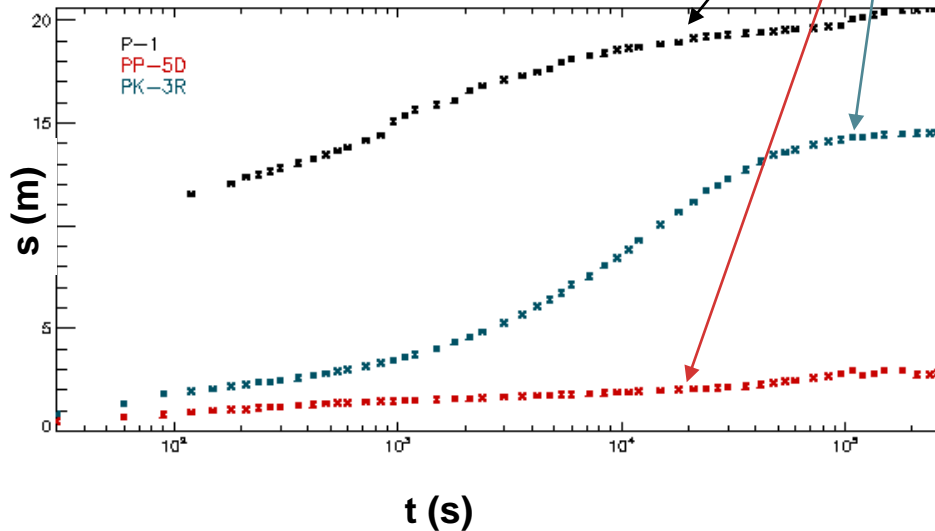


Fig. 2: Semi-log plot of the s.

" The new way " *

Drawdown-log derivative
ds/dlogt

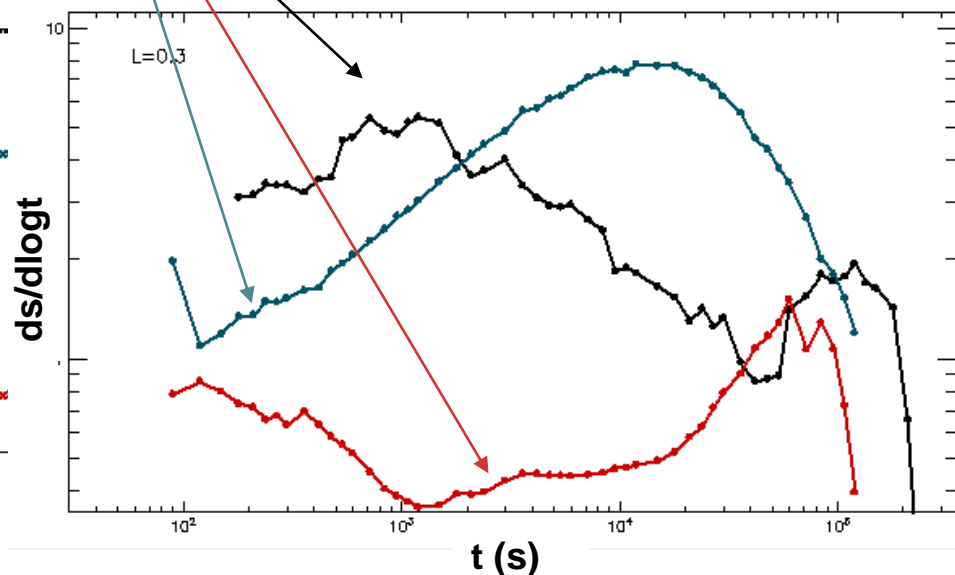


Fig. 3: Log-log plot of ds/dlogt (Bourdet et al., 1989).

Much more sensitive signal
...But the physical interpretation = still enigmatic

* *Mattar (1997)*

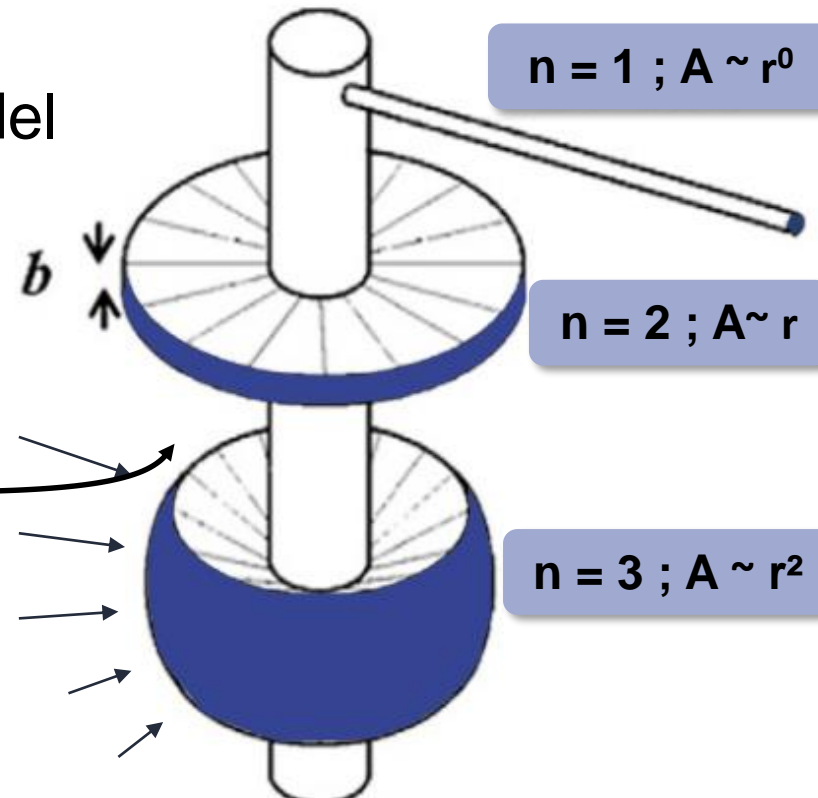


1.3 Hydraulic interpretation of $ds/d\log t$

Generalized Radial flow (GRF) Model
(Barker, 1988)

$$A(r) \sim r^{n-1}$$

n reflects the **geometry of the pressure wave** when it diffused through the aquifer



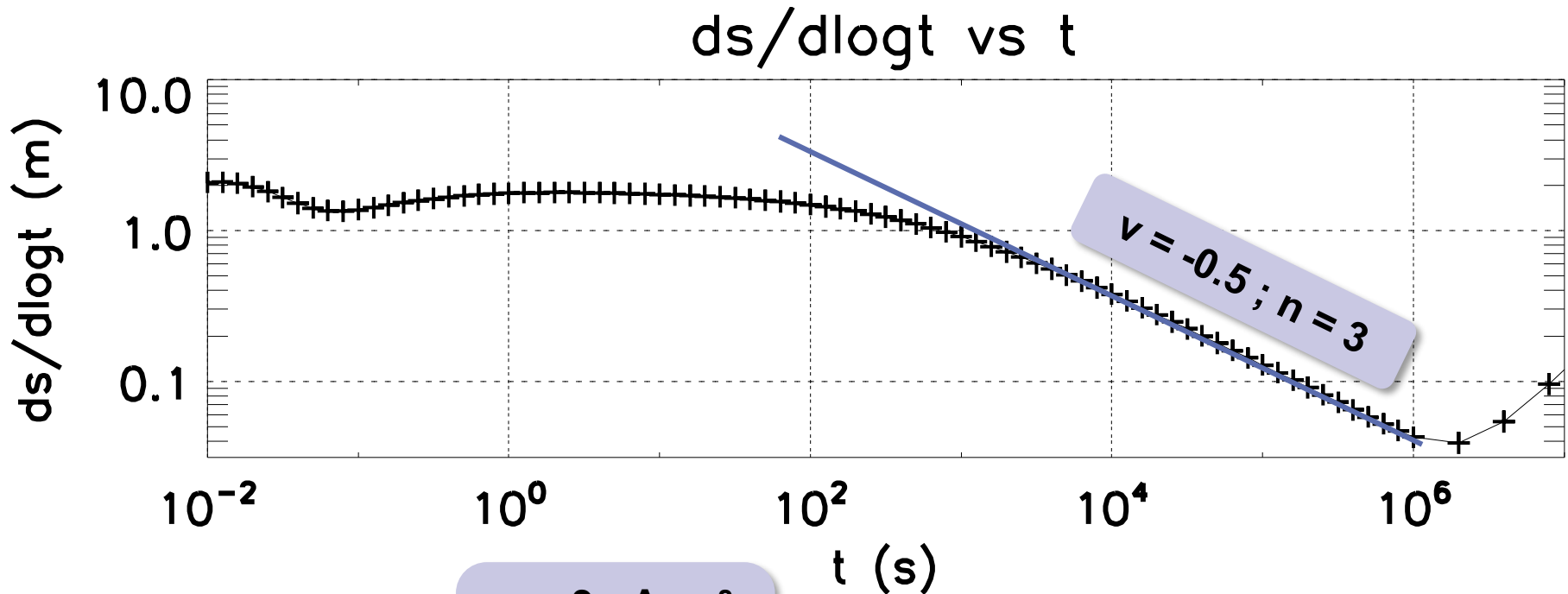
"Flow geometry combined to the hydraulic properties of the aquifer"
(Beauheim et Roberts, 1998).

$A(r)$: cross-flow area
 r : radial distance from the well (m)
 n : flow dimension parameter (= **flow regime**)

1.3 Hydraulic interpretation of $ds/d\log t$

How to estimate n from transient well test data?

$$n = 2.(1-v)$$



n : flow dimension
 v : slope of $ds/d\log t$

2. Objective and issue of the study



Objective

To develop advanced tools of interpretation of pumping tests based on $ds/d\log t$ signal and Barker's theory

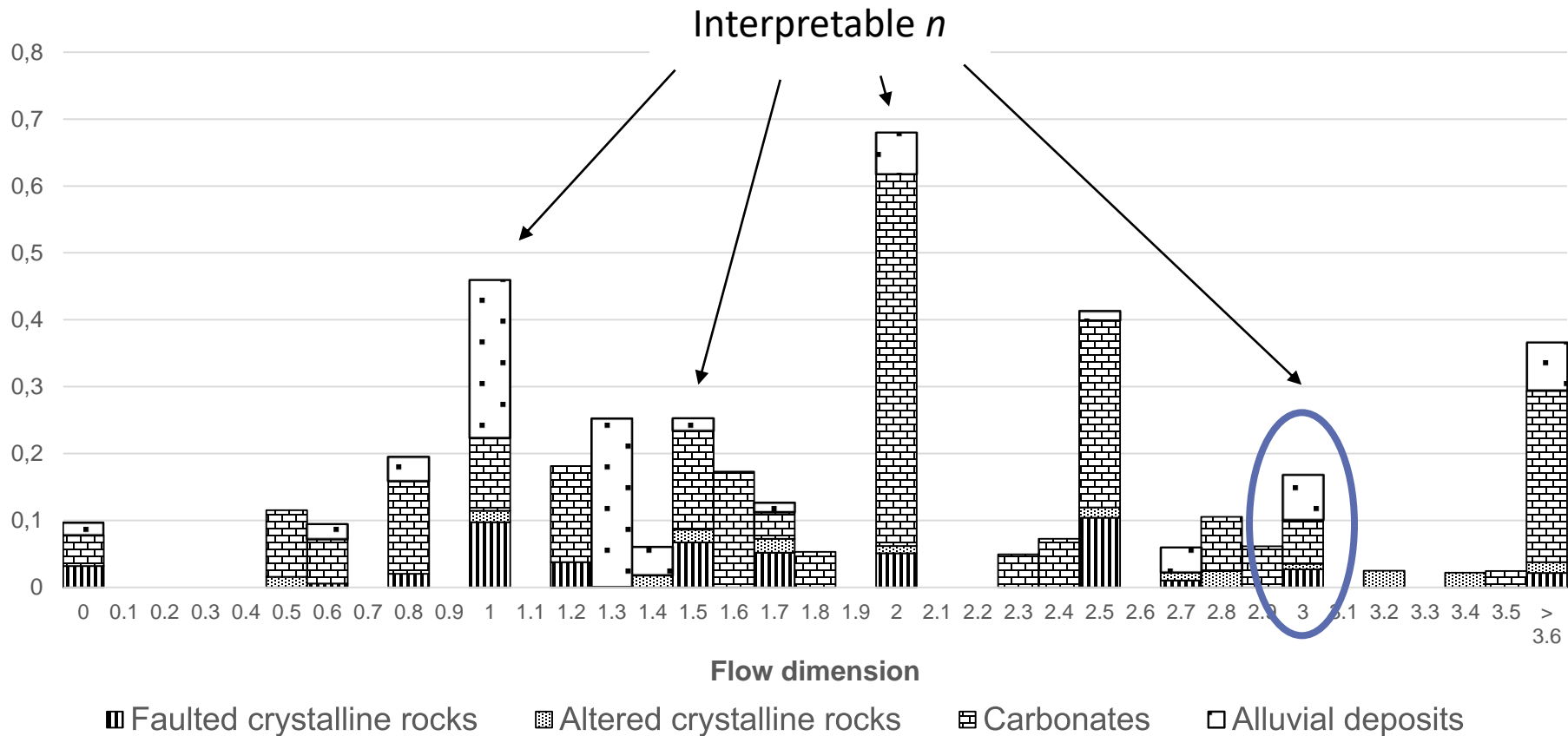
Issue

What are the conceptual models producing a spherical flow regime?

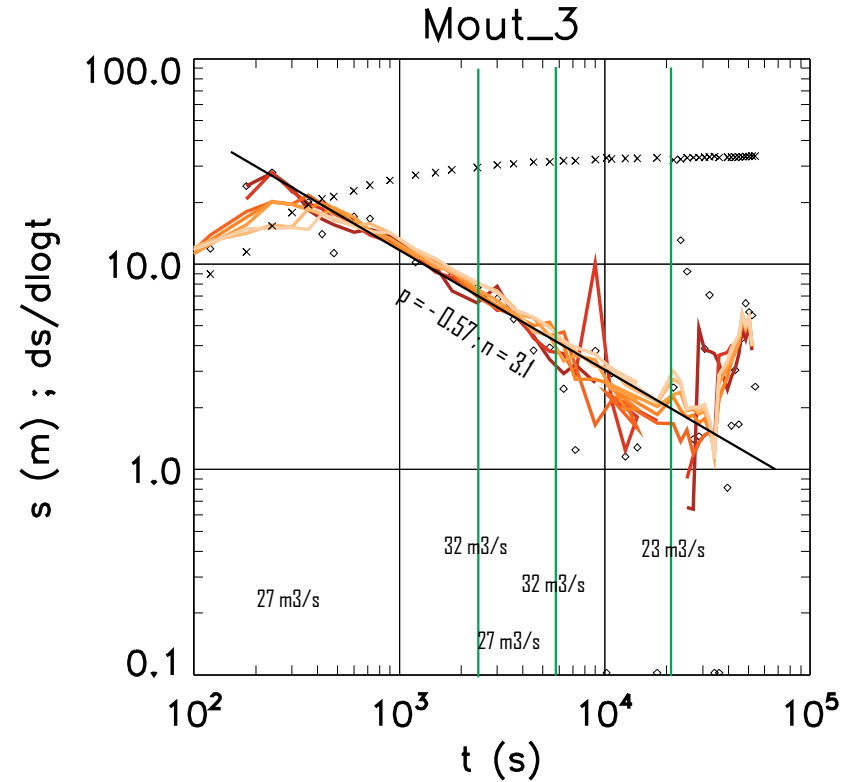
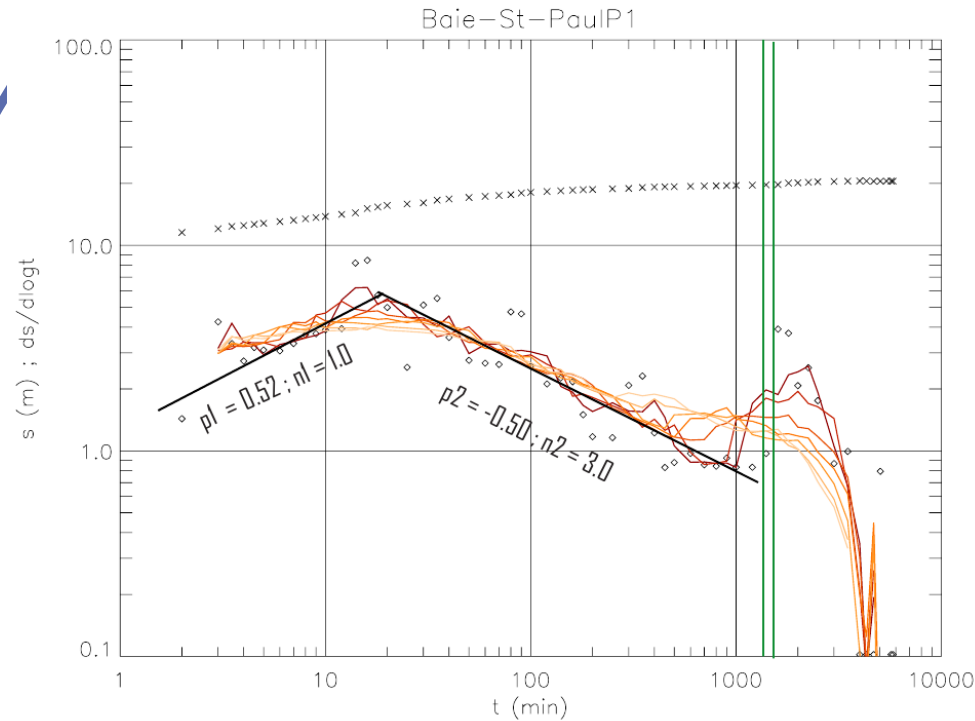
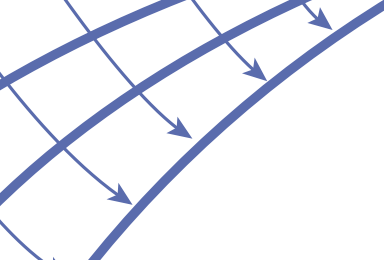
1.4 Field data: observation of n in nature

Previous study:

Statistical occurrence of flow dimension in various geological environments \rightarrow n distribution in nature.



1.4 Field data: spherical flow regime



3. Methodology



3.1 The model: HydroGeoSphere (HGS)

HydroGeoSphere (*Therrien et al., 2010, Aquanty, 2015*)

HGS = Spatially distributed and physically-based 3D modelling software.

Numerical implementation:

For sub-surface and saturated flow:

Diffusivity equation

$$\vec{\nabla}(\bar{\bar{K}}(x, t)\vec{\nabla}h) = S_s(x, t)\frac{\partial h}{\partial t} \pm f(x, t)$$

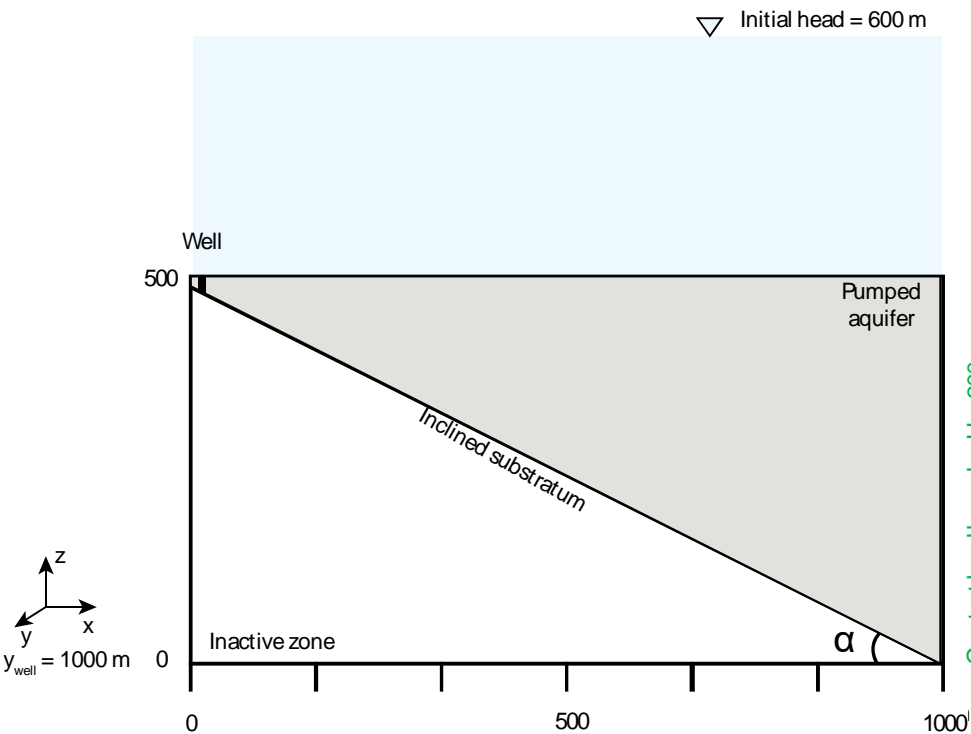
Discretization :

- Finite element method,
- Control-volume finite element method.

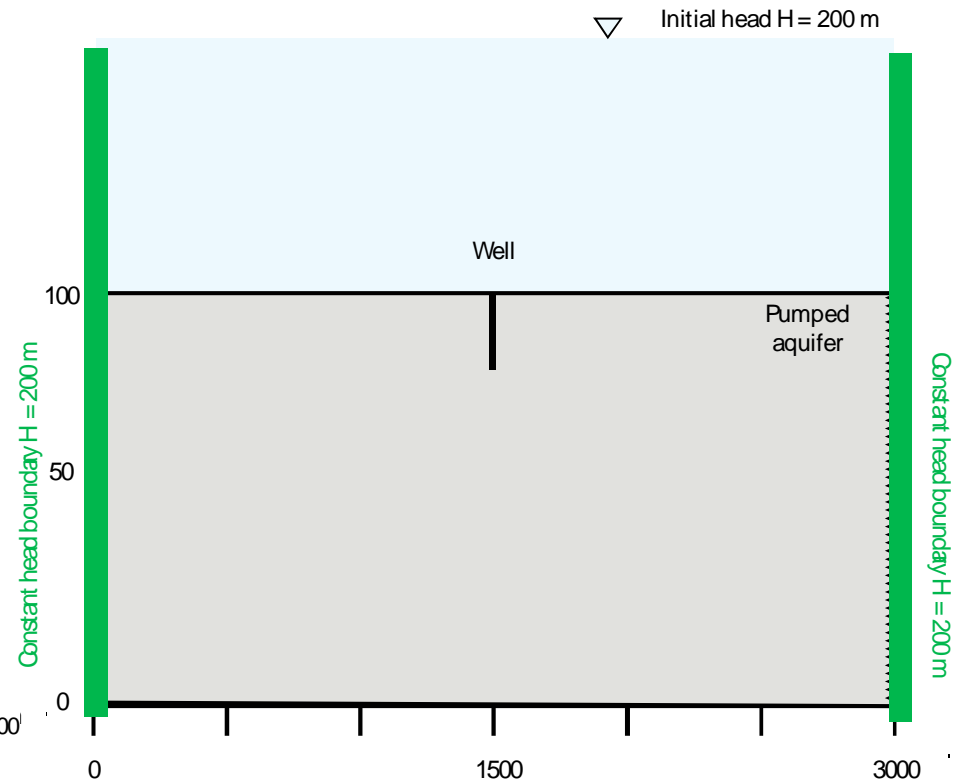
K : Hydraulic conductivity (m/s)
 S_s : Specific storage
 h : hydraulic head (m)

3.2 The conceptual models

Inclined substratum



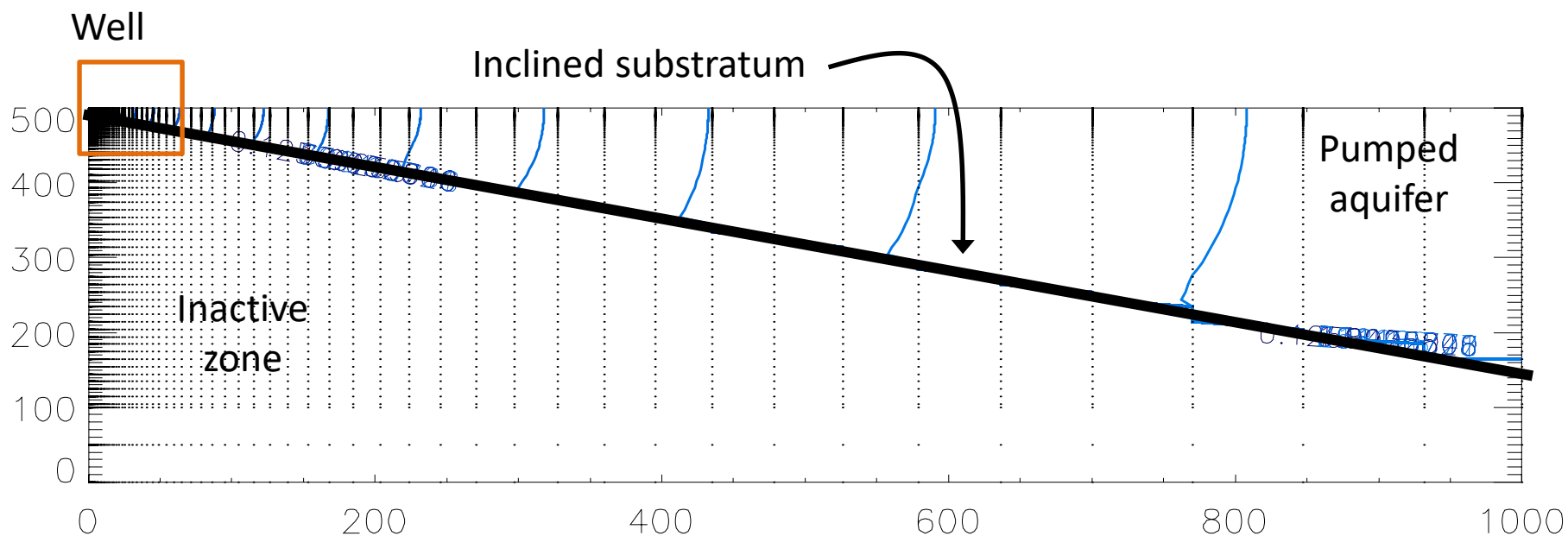
Partially penetrated aquifer



4. Results

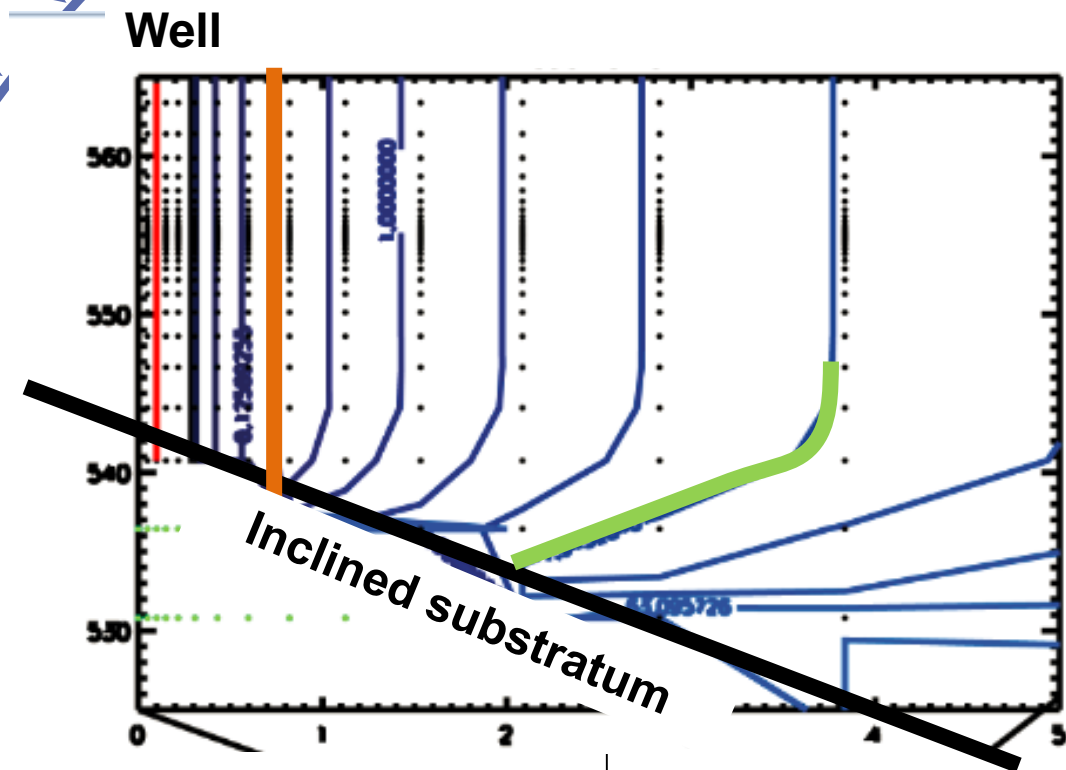


4.1 Propagation of frontal the equipotential surface



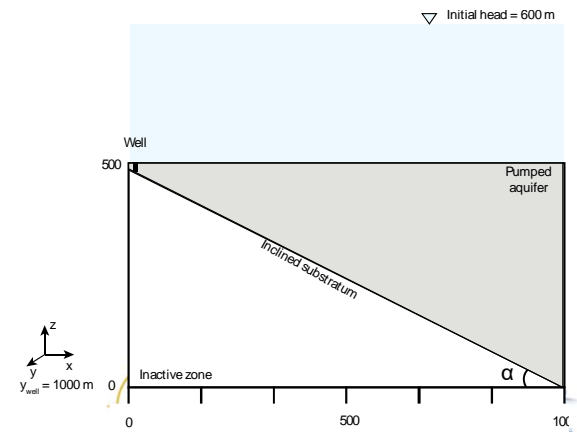
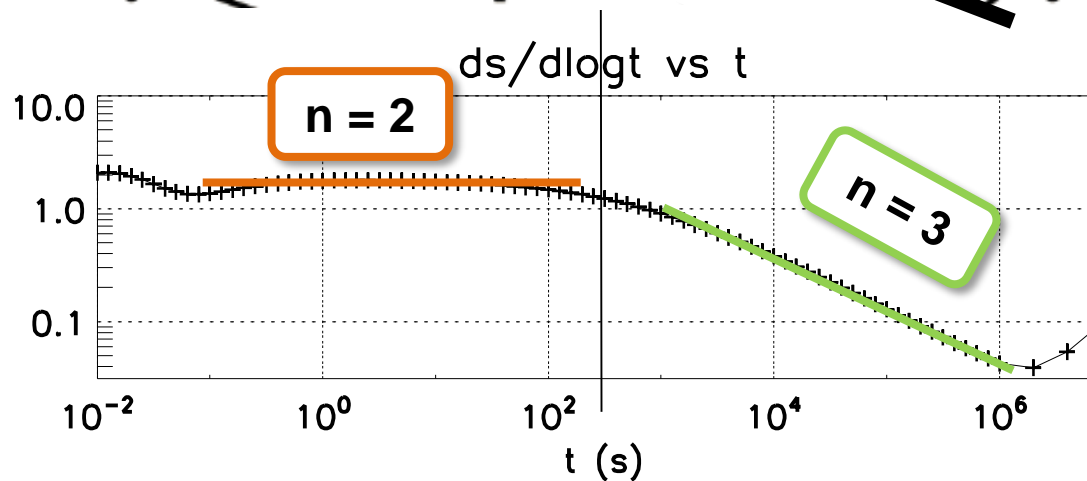
Front pulse diffusion – $y=1000.00$

4.1 Propagation of frontal the equipotential surface



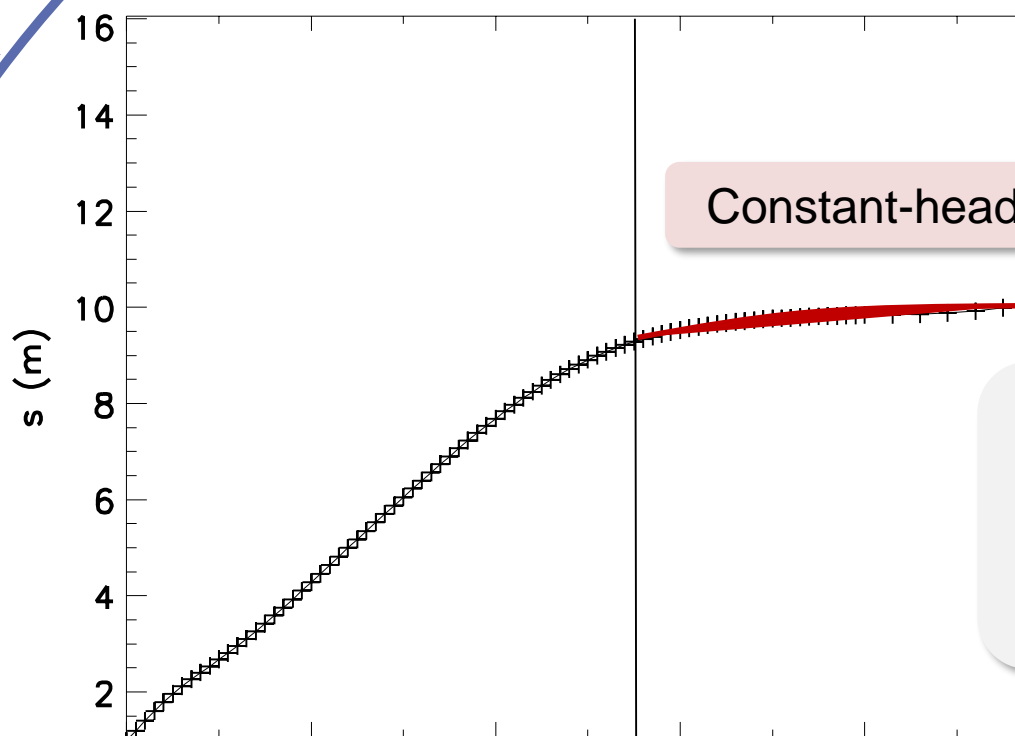
$A \sim r$
Early cylindrical-radial flow regime

$A \sim r^2$
Spherical flow regime

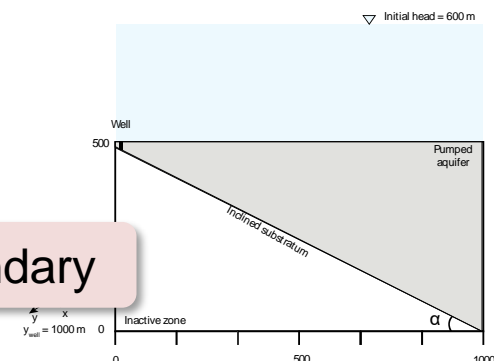


4.2 The $ds/d\log t$ signal: inclined substratum

s vs t

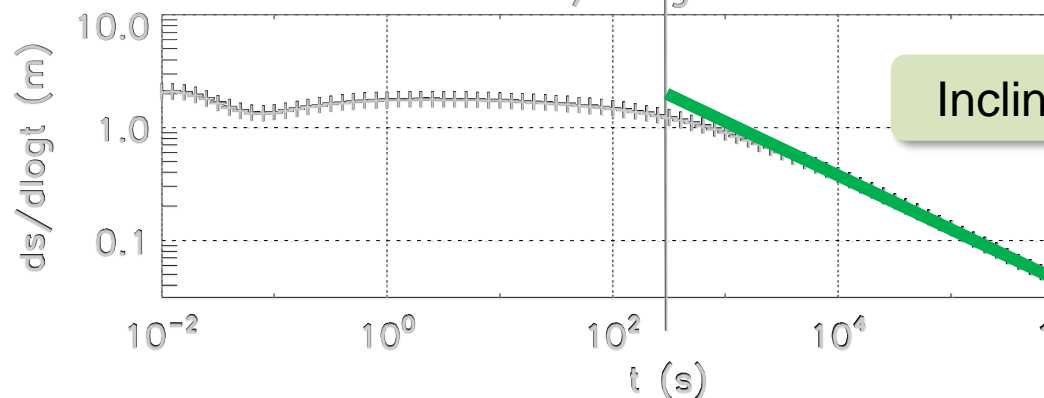


Constant-head hydraulic boundary



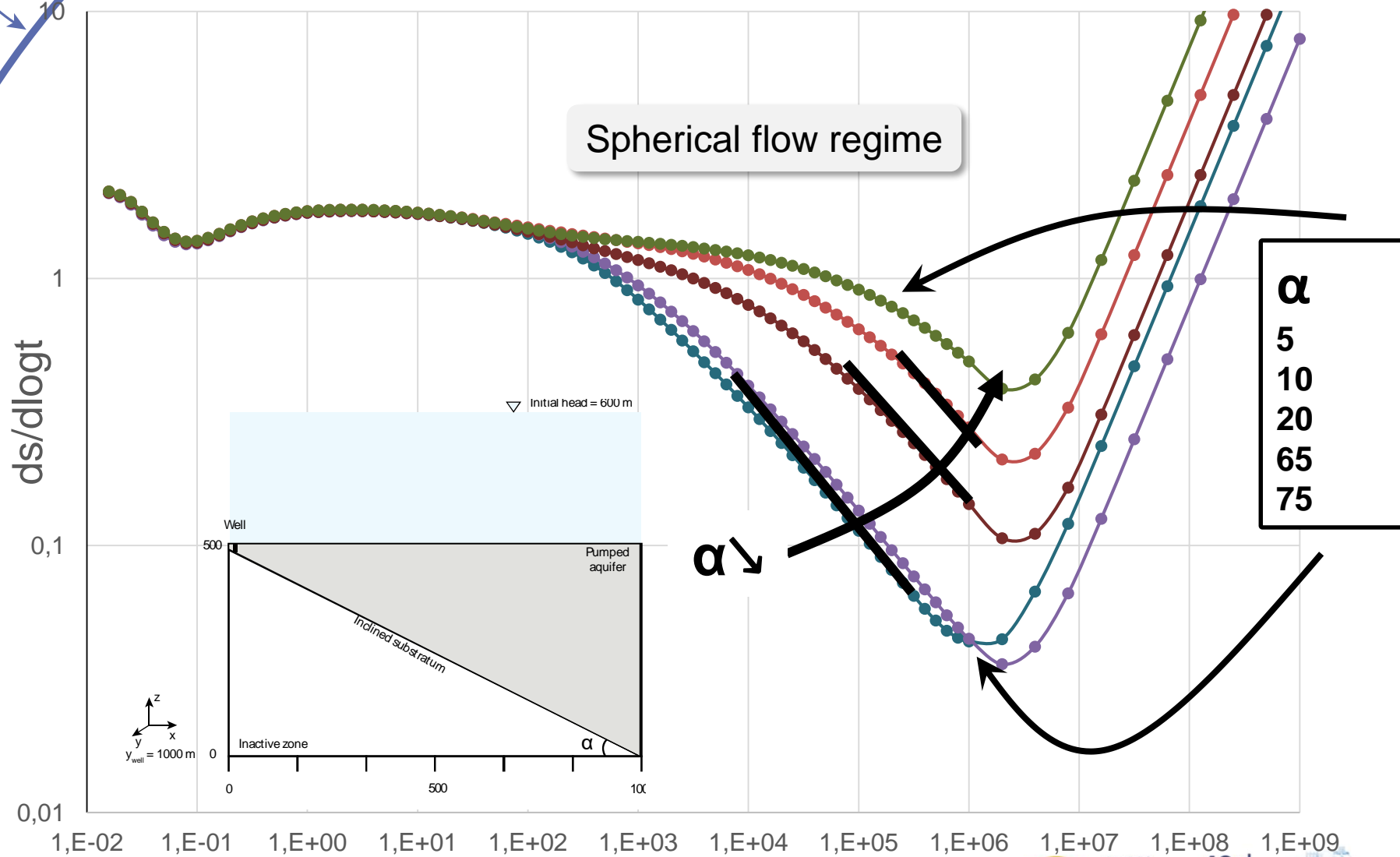
Interpretation of the hydraulic signal and detection of the boundary conditions = more reliable

$ds/d\log t$ vs t



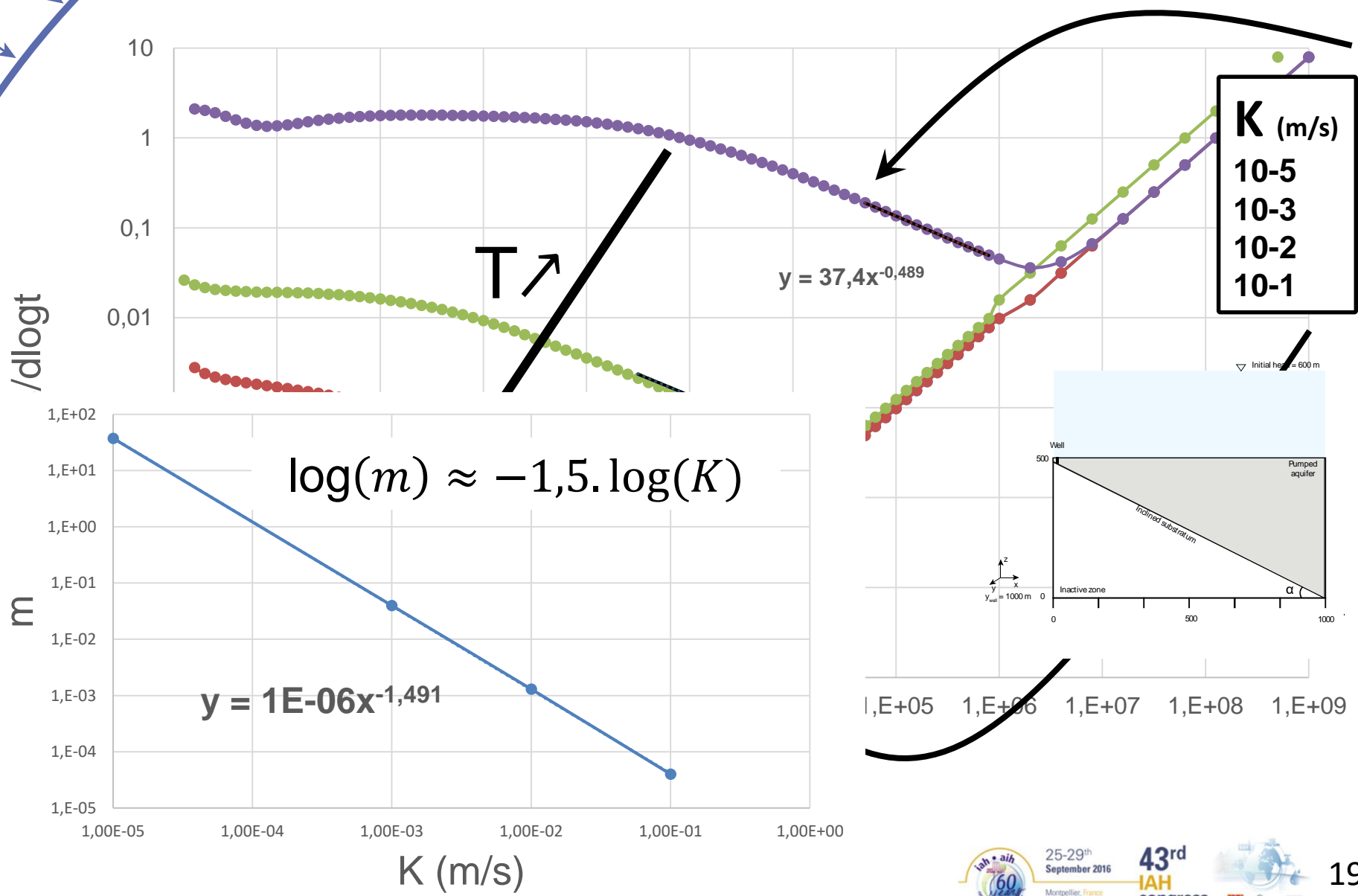
Inclined substratum

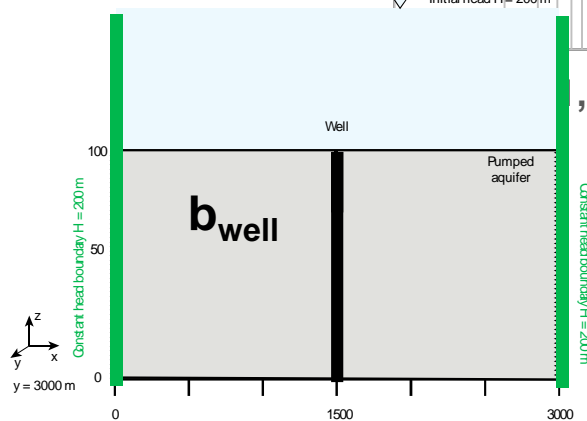
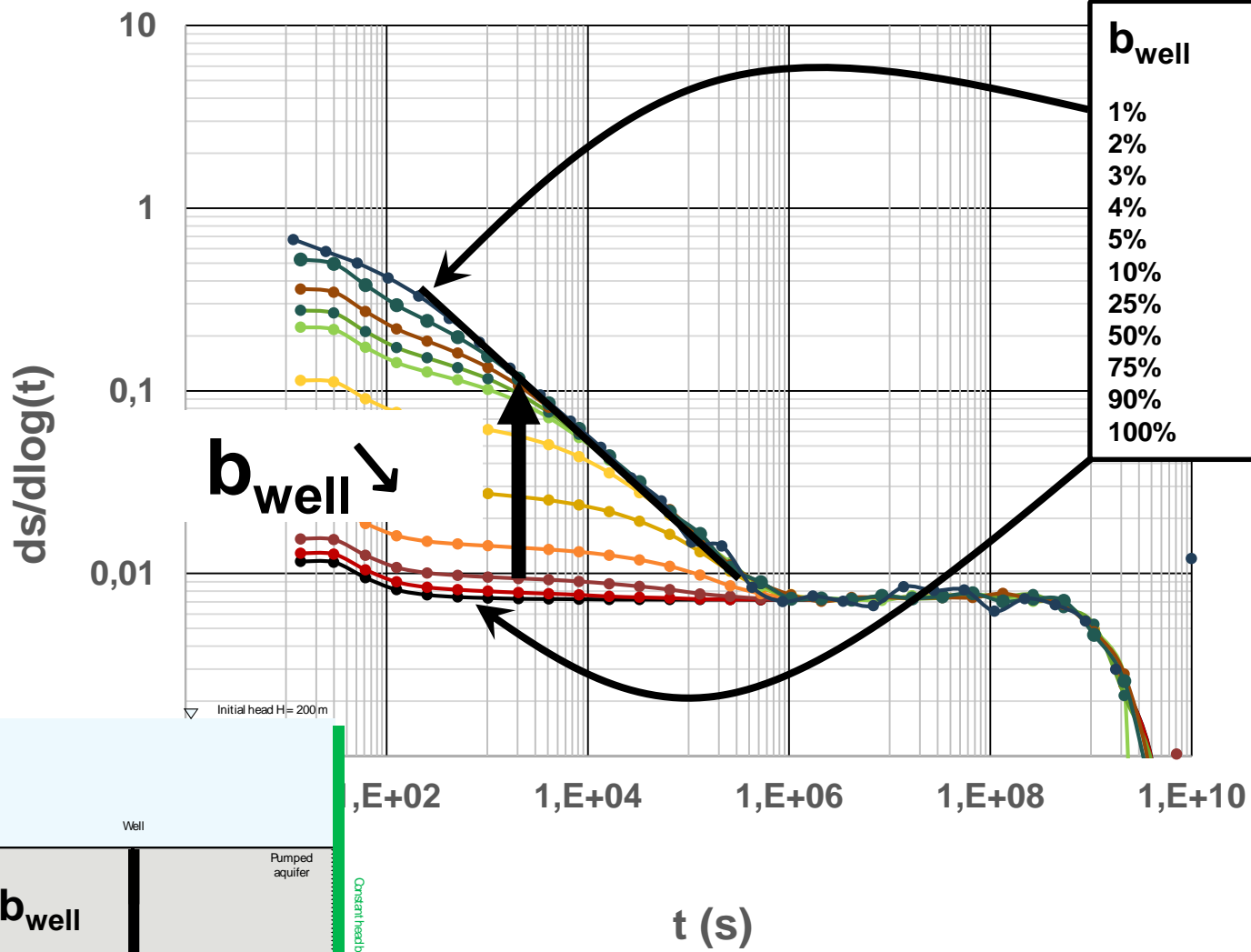
4.2 The $ds/d\log t$ signal: inclined substratum



α : slope of the inclined substratum

4.2 The $ds/d\log t$ signal: inclined substratum





5. Discussion and conclusion



The derivative approach doesn't need more data, but it gives much more information!

- qualitative: analysis of flow geometry
- quantitative: estimation of hydraulic properties with more reliability

Sensitivity analysis \rightarrow empirical equation \rightarrow estimation of K from a $ds/d\log t$ curve fitting

Non-uniqueness of the flow regimes!!!

Partially penetrated aquifer $\rightarrow n = 3$

An inclined substratum $\rightarrow n = 3$

Geological settings = essential to interpret a pumping test!
Sequences of $n =$ help to reduce the non uniqueness!

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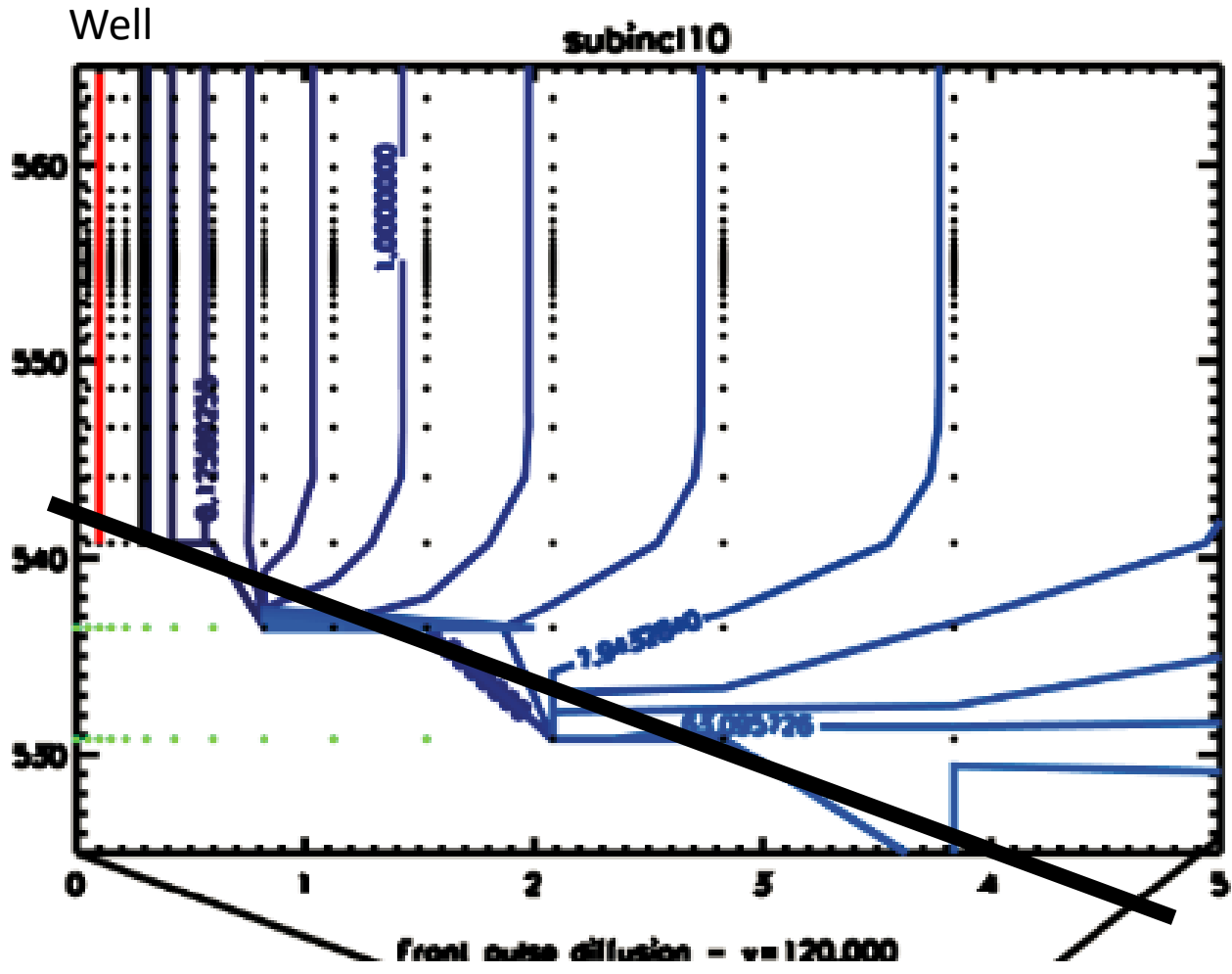
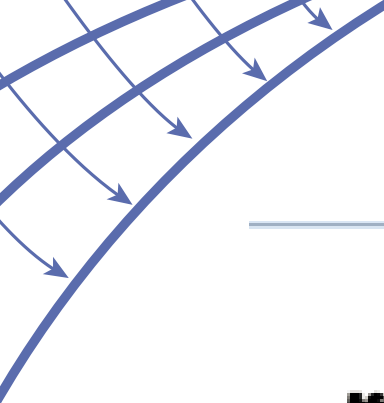
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Algorithm of Bourdet *et al.* (1989)

$$\frac{dS_i}{dX_i} = \left(\frac{\Delta s_1}{\Delta X_1} \Delta X_2 + \frac{\Delta s_2}{\Delta X_2} \Delta X_1 \right) / (\Delta X_1 + \Delta X_2)$$

$$X = \log(t)$$

$$\Delta X_1 = X_i - X_1$$

$$\Delta s_1 = s_i - s_1$$

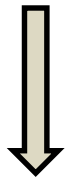
$$\Delta s_2 = s_i - s_2$$

$$\Delta X_2 = X_i - X_2$$

Estimation de n

Generalized diffusivity equation

$$\frac{K}{r^{n-1}} \frac{\partial}{\partial r} \left(r^{n-1} \frac{\partial h}{\partial r} \right) = S_s \frac{\partial h}{\partial t}$$



Laplace transformation

Hyp:

Constant head head at the boundaries

Initial head = 0 m at the beginning

General solution

$$h(r,t) = \frac{Qr^{2v}}{4\pi^{1-v} Kb^{3-n}} \Gamma(-v,u) \quad v \neq 0$$

avec, $u = \frac{S_s r^2}{4Kt}$ et, $v = 1 - \frac{n}{2}$

$$\Gamma(a,x) = \int_x^\infty t^{a-1} e^{-t} dt$$

Estimation de n

For a little u,

$$h(r,t) = \frac{Q}{4\pi^{1-v} K b^{3-n} \nu} \left(\left(\frac{4Kt}{S_s} \right)^v - \Gamma(1-v) r^{2v} \right) \quad \nu \neq 0$$

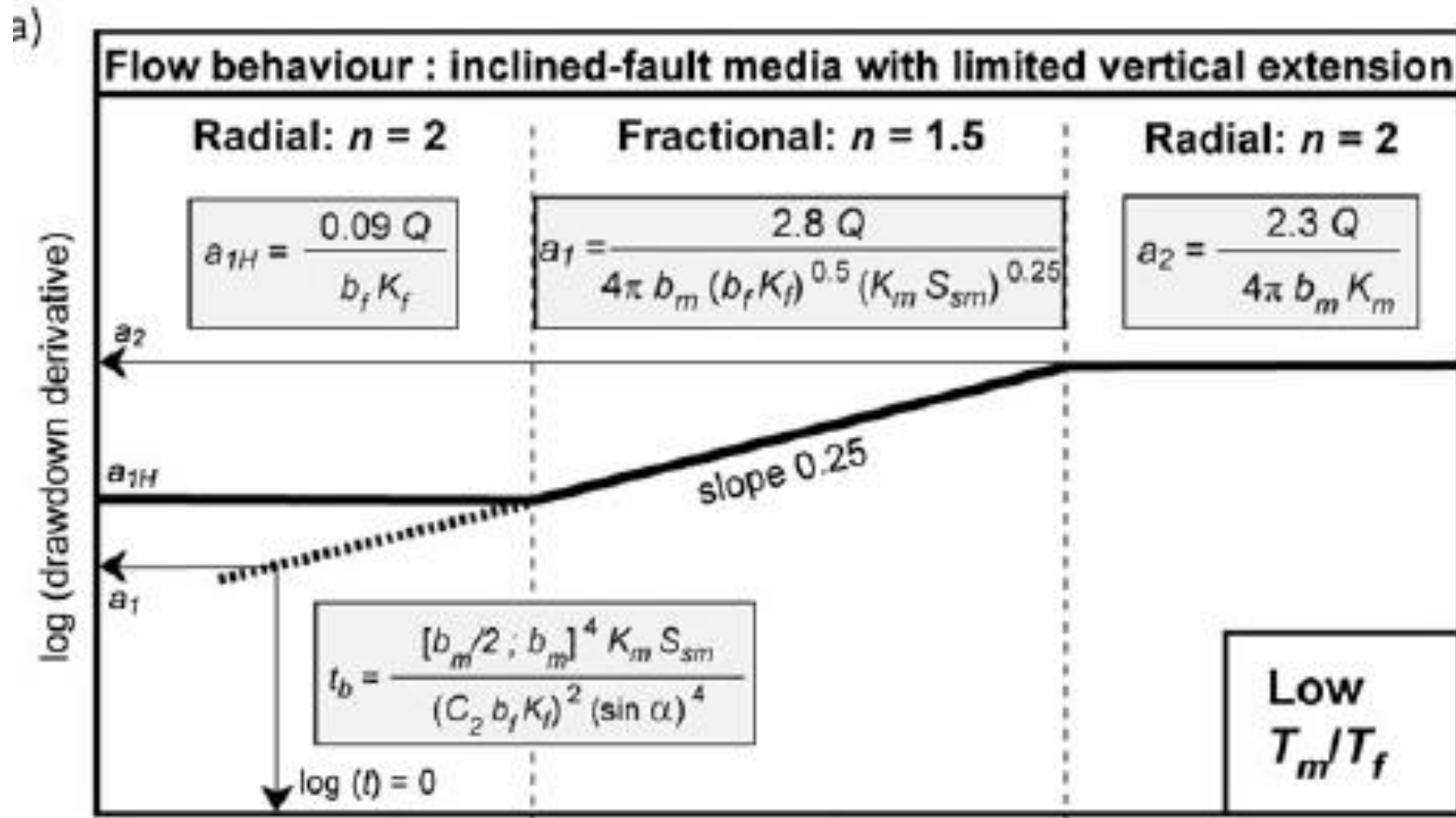
$$h(t) = Ct^v + C'$$

$$\frac{dh}{d \log t} = t \frac{dh}{dt} = 2,3 . C . \nu t^v$$

$$n = 2(1 - p)$$

Slope of ds/dlogt

Rafini, S., & Larocque, M. (2012). Numerical modeling of the hydraulic signatures of horizontal and inclined faults. Hydrogeology Journal, 20(2), 337-350



1.4 Field data: spherical flow regime

Geology: Granitic sand

Mout_3

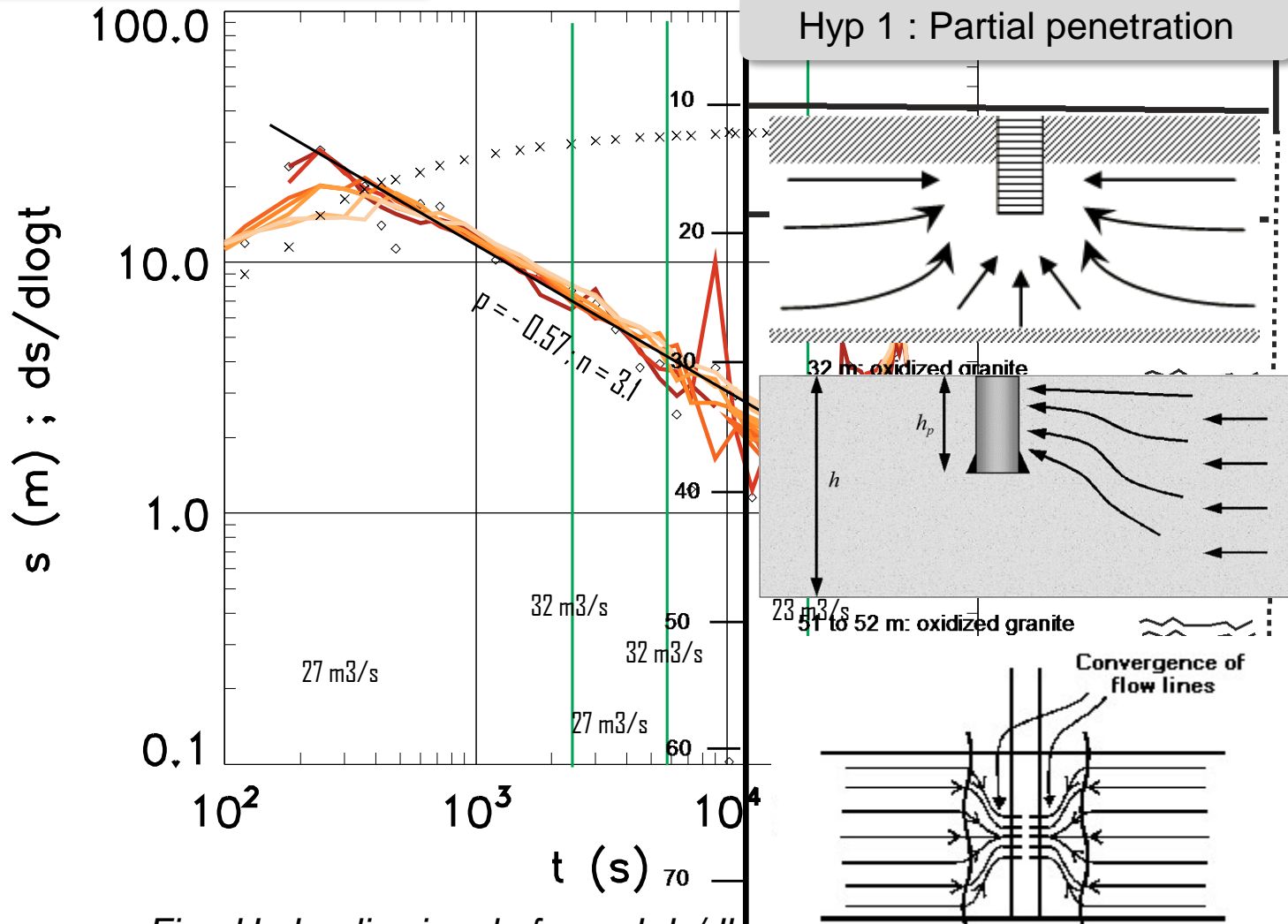


Fig.: Hydraulic signal of s and $ds/d\log t$
 Vendée, Pays-de-la-Loire, France.

Altered granitic aquifer

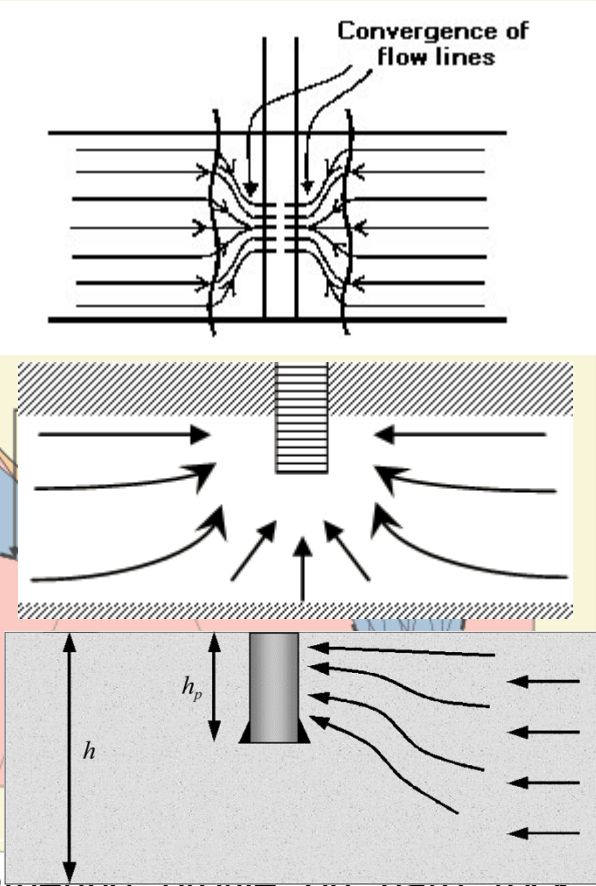
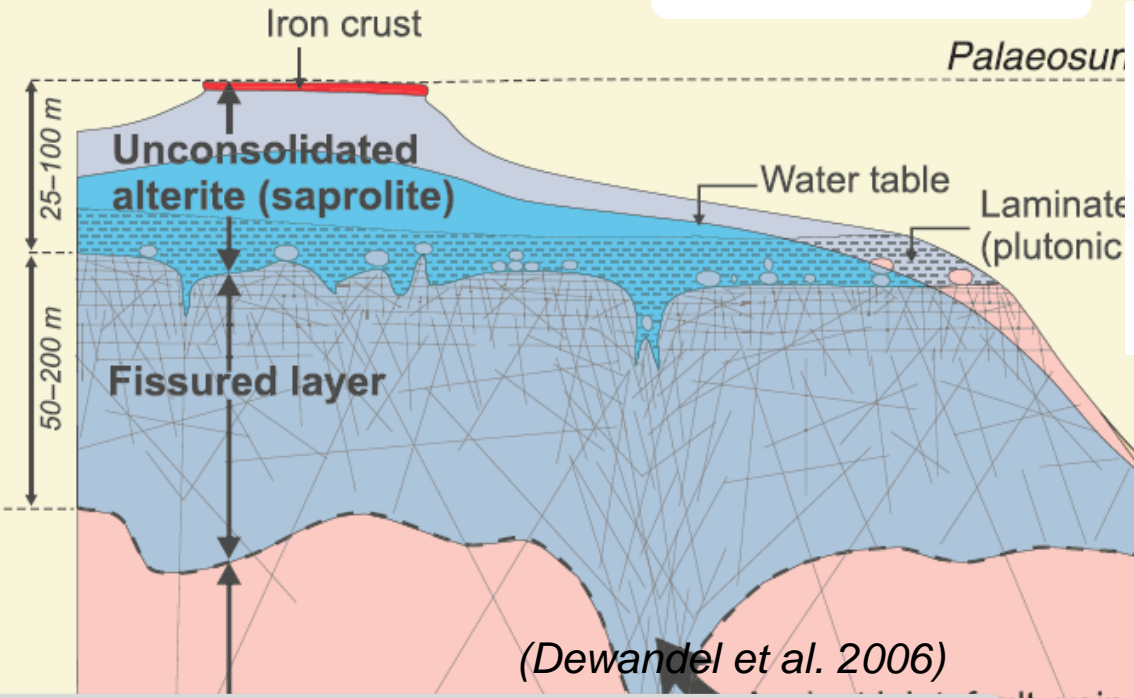
Hydrogeological interpretation

Spherical flow

Leaky effects

and/or

Wellbore effects



Water supply from the weathered horizon to the fissured rock (Dewandel et al. 2006).

Fig. 13: Conceptual model of a partly eroded palaeo-weathering profile on hard rock (Dewandel et al. 2006). Fig. 14: Illustrations of a partial penetration / completion.

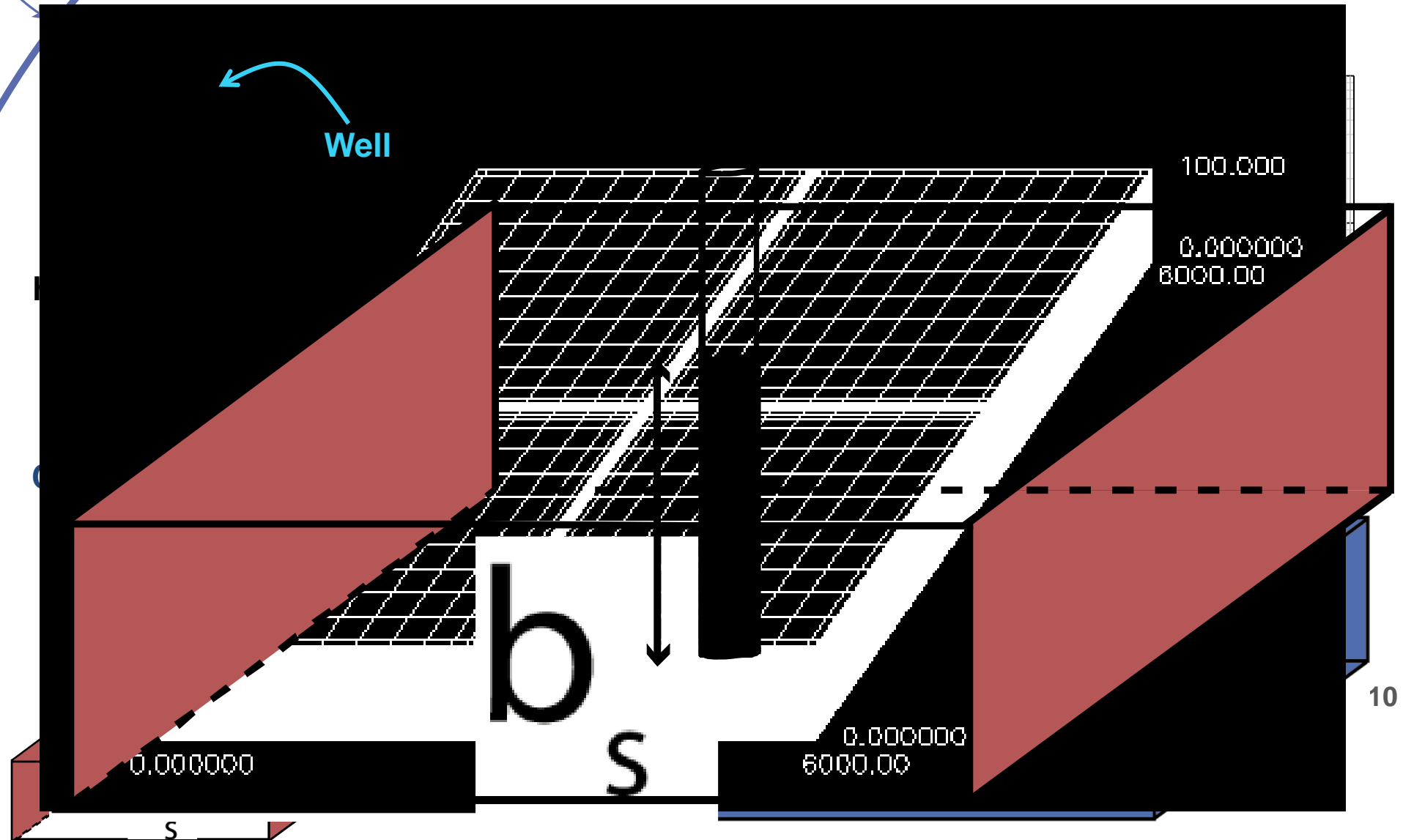
Partial penetration or Partial completion

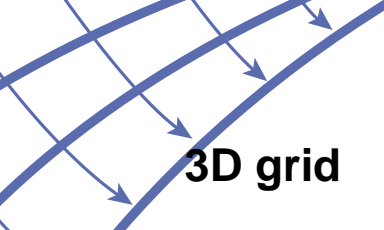
<http://www.fekete.com/>
<http://nptel.ac.in/courses/105103026/20>
<http://petrowiki.org/>

3.2 The conceptual model 1: inclined substratum

3D grid

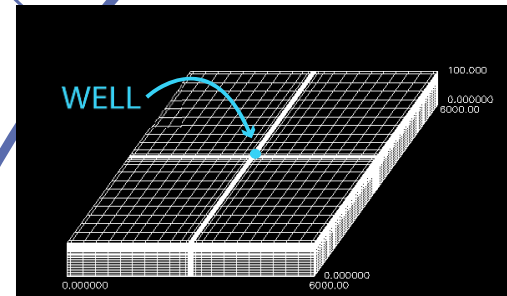
Well





3D grid

Screen thickness b_s (m)



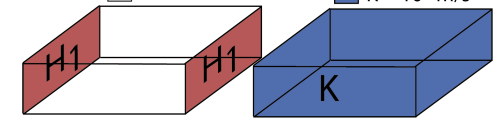
WELL

Boundaries and hydraulic properties

$H_1 = 200$ m

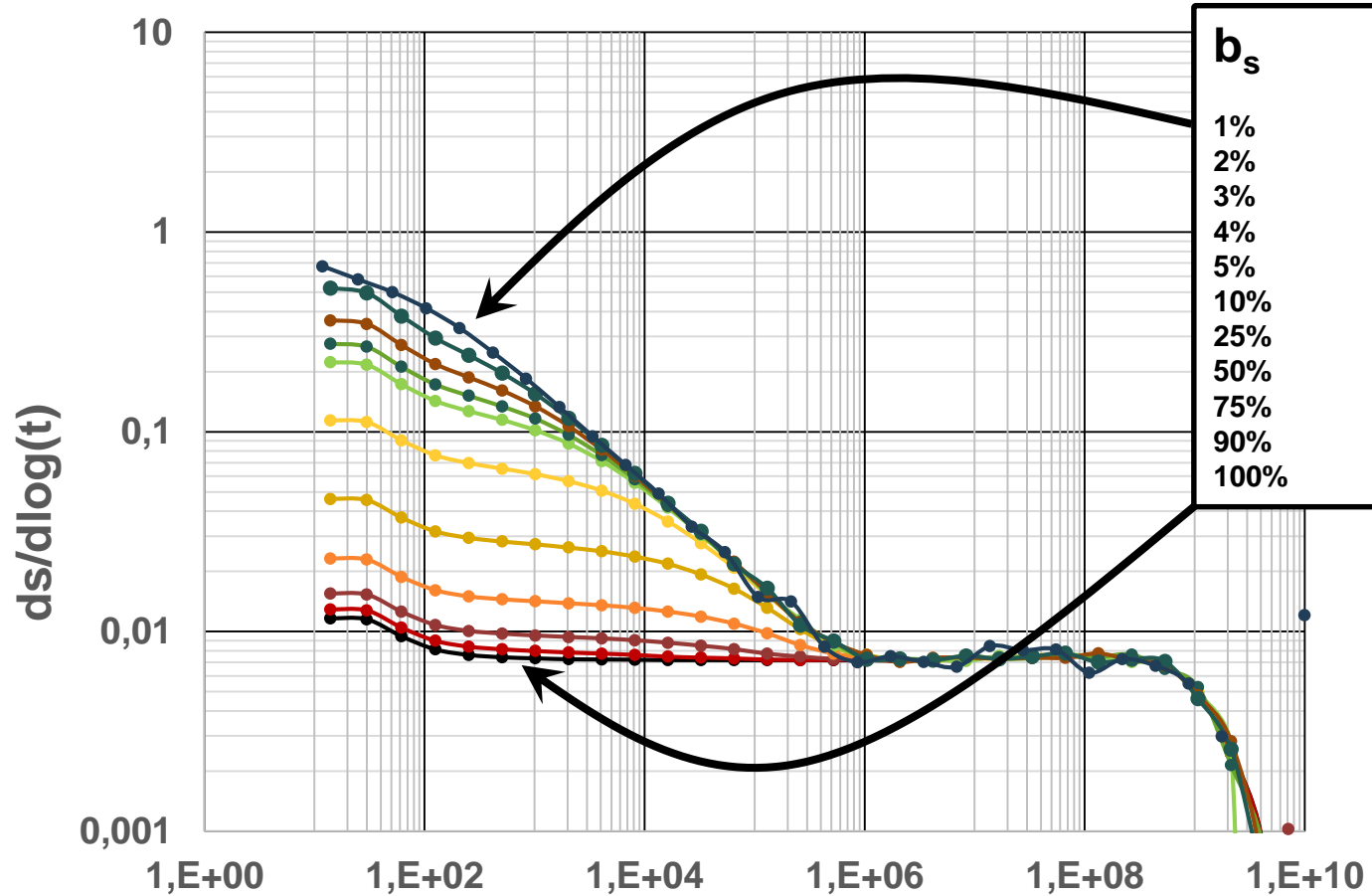
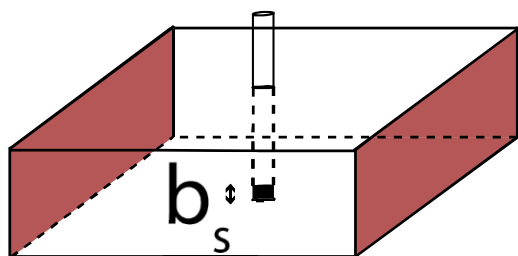
No flow

$K = 10^{-4}$ m/s



Confined aquifer

Tested parameter



t (s)



25-29th
September 2016

Montpellier, France
CORUM CONFERENCE CENTER

43rd
IAH
congress



1.4 Field data: spherical flow regime

Geology: clay; sand; rock

Longue-Rive : P1

Ouvrir

Info format Desc. Remort.

Correction de Bourdet

0.3 L min
0.2 L incr
1.2 L max

Débit pompage m3/s 0.0

Affichage plusieurs puits
 N_{nm} en L/(r²·2)
 N_{nm} en s/(r²·(2-n))
n = 0.00

Courbes

Extr. image
Extr. data

Ouvrir fiche
Enreg. fiche

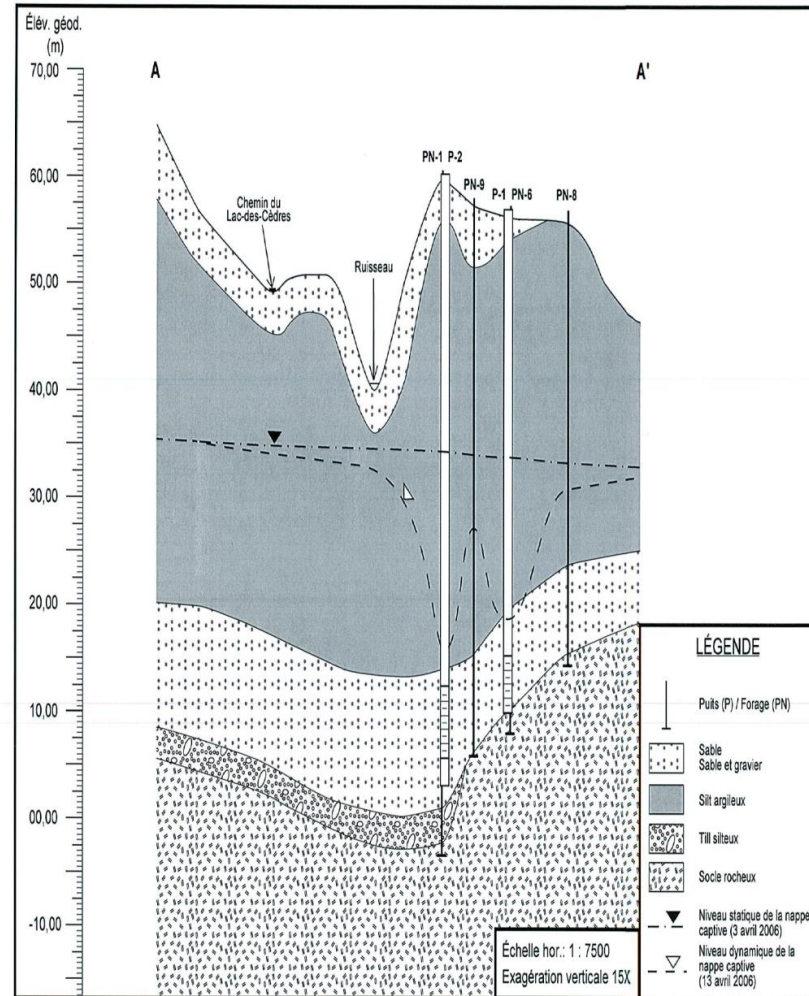
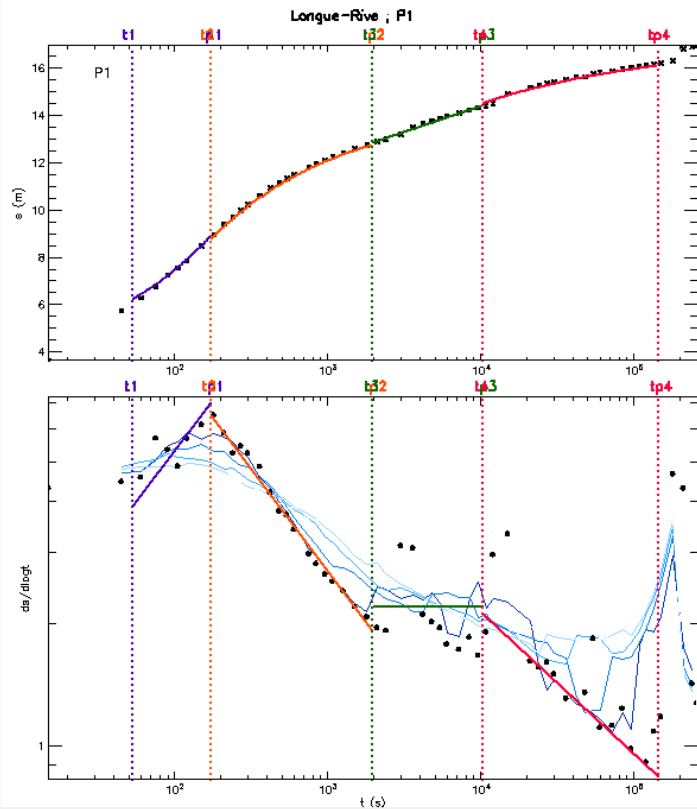


Figure 16. Coupe hydrostratigraphique longitudinale A - A'